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Description

<u>Pressure-sensitive adhesive article with at least one layer of an electrically</u> conductive adhesive mass and method for production thereof

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The invention relates to a method of producing a pressure-sensitive adhesive article having at least one layer of a thermally conductive pressure-sensitive adhesive (PSA) mass, and also to a pressure-sensitive adhesive article obtainable in this way, particularly for adhesive bonds in the field of electrical and electronic components.

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In the age of computerization electrically conductive PSAs are being used more and more for bonding electrodes or electromagnetic components. The objective is to maintain the electrical conductivity and to avoid electrical sparkovers.

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In general for these applications electrically conductive acrylate PSA tapes are used. The electrical conductivity can be achieved by two different methods. On the one hand, conductive films or fabrics are used; on the other hand, the PSA is modified by electrically conductive components and so itself becomes electrically conductive.

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Examples of electrically conductive carrier materials are specified for example in US 5,939,190 and 6,235,385 and in the patents cited therein.

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Electrically conductive acrylate PSAs as well have already been known for a long time. Thus it is described in US 4,113,981 how electrical conductivity can be achieved by adding metal powder or SiC powder. Through the degree of filling the conductivity can be varied. Furthermore, when the mass is included between two electrodes, electrical conductivity only in the z direction is obtained by a limitation to 30%.

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In US 5,300,340 silverized glass beads and metal beads are mixed into a PSA. The diameter of these beads is at least exactly the same size as the layer thickness of the

PSA. The electrical conductivity is therefore brought about by the direct contact of the conductive beads with the conductive substances to be bonded (electrodes, for example).

US 5,620,795 and US 6,126,865 use polyacrylates of defined comonomer composition as electrically conductive acrylate PSAs. The comonomer composition of the polyacrylates is chosen such that highly nonpolar resins are compatible with the polyacrylate and therefore it is possible with the electrically conductive PSA to realize high bond strengths on nonpolar surfaces.

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As a result of the miniaturization within the electronics/computer industry, however, the requirements imposed on electrically conductive PSAs are becoming evermore stringent. The electrical components to be bonded are becoming smaller and smaller in size, so that in many cases only diecuts can still be used for the bond. Furthermore, there is continual reduction in the spacing of the circuits, so that electrically conductive PSAs are needed that possess only very low flow behavior in a particular direction (to the next electrically conductive component).

It is an object of the invention, therefore, to provide electrically conductive pressuresensitive adhesives, in particular for the electrical and electronics industry, with which the disadvantages in the prior art are avoided and, in particular, the outward swelling or outward flow of the pressure-sensitive adhesive at the edge of the bond is reliably avoided.

This object is achieved, surprisingly and in a manner not foreseeable for the skilled worker, by a method by means of which anisotropic, oriented pressure-sensitive adhesives with a shrinkback of at least 3% with coating onto a carrier (including, where appropriate, a temporary carrier from which the pressure-sensitive adhesive can be removed again) are obtained, and also by associated pressure-sensitive adhesive articles obtained in this way. Developments of the invention are characterized in the dependent claims.

The achievement of the object of the invention encompasses a method of producing a pressure-sensitive adhesive article for bonding electrical or electronic parts which has at least one layer of an electrically conductive pressure-sensitive adhesive, i.e., a pressure-

sensitive adhesive based on polyacrylates and/or polymethacrylates with or without further comonomers, wherein a layer which is anisotropic at least in respect of one property is produced from the electrically conductive pressure-sensitive adhesive in a coating process by stretching, drawing or compressing, said layer possessing in at least one direction along the plane of the layer a shrinkback of at least 3% in respect of the longitudinal extent of the layer, measured by a shrinkback measurement according to test B on the free film.

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Anisotropy means that at least one property of the pressure-sensitive adhesive in one spatial direction within the layer of the PSA differs from the same property in at least one other direction; in other words, anisotropic properties are vectorial and not uniform within the material.

The pressure-sensitive adhesive preferably possesses an orientation as known as such, i.e., a preferential direction within the polymer structure.

The coating process may be for example a hotmelt roll coating process, a melt die coating process or an extrusion coating process.

In an alternative embodiment of the invention the coating process is a conventional coating process, from solution for example, in which coating is followed by stretching or drawing, preferably on a stretchable carrier.

The electrically conductive pressure-sensitive adhesive can be coated by the coating process onto one or both sides of a sheetlike or tapelike carrier, which may also be a transfer tape or a release liner.

Pressure-sensitive adhesives which can be used in accordance with the invention

In accordance with the invention, pressure-sensitive adhesives having a resilience or else anisotropically oriented or simply "oriented" pressure-sensitive adhesives are used.

Anisotropically oriented PSAs possess a tendency, after stretching in a given direction, to move back into the initial state as a result of their 'entropy-elastic' behavior.

As electrically conductive PSAs with a resilience it is preferred to use (meth)acrylate PSAs.

Preference in the sense of the invention is given to a pressure-sensitive adhesive which is obtainable by free-radical addition polymerization, where

 the pressure-sensitive adhesive is based to an extent of at least 50% by weight on at least one acrylic monomer from the group of the compounds of the following general formula:

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where R_1 = H or CH_3 and the radical R_2 = H or CH_3 or is selected from the group of branched or unbranched, saturated alkyl groups having 2 – 30 carbon atoms.

- the average molecular weight M_w of the pressure-sensitive adhesive is at least 200 000 g/mol,
 - the pressure-sensitive adhesive, applied to a carrier, possesses a preferential direction which can be determined by test B via the shrinkback in the free film and is at least greater than 3%.
- which comprises an effective fraction of at least one electrically conductive
 component

The monomers are preferably chosen such that the resulting polymers can be used, at room temperature or higher temperatures, as PSAs, particularly such that the resulting polymers possess pressure-sensitive adhesion properties in accordance with the "Handbook of Pressure Sensitive Adhesive Technology" by Donatas Satas (van Nostrand, New York 1989).

In a further inventive embodiment the comonomer composition is chosen such that the PSAs can be used as heat-activable PSAs.

The polymers used with preference as electrically conductive PSAs with resilience can be obtained preferably by polymerizing a monomer mixture which is composed of acrylic esters and/or methacrylic esters and/or the free acids thereof, with the formula $CH_2 = CH(R_1)(COOR_2)$, where R_1 is H or CH_3 and R_2 is an alkyl chain having 1-20 carbon atoms or is H.

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The molar masses M_w of the polyacrylates used amount preferably to M_w $\geq 200~000~g/mol$.

In one way which is greatly preferred, acrylic or methacrylic monomers are used which are composed of acrylic and methacrylic esters having alkyl groups comprising 4 to 14 carbon atoms, and preferably comprise 4 to 9 carbon atoms. Specific examples, without wishing to be restricted by this enumeration, are methyl acrylate, methyl methacrylate, ethyl acrylate, n-butyl acrylate, n-butyl methacrylate, n-pentyl acrylate, n-hexyl acrylate, n-hexyl acrylate, n-heptyl acrylate, n-octyl methacrylate, n-nonyl acrylate, lauryl acrylate, stearyl acrylate, behenyl acrylate, and the branched isomers thereof, such as isobutyl acrylate, 2-ethylhexyl acrylate, 2-ethylhexyl methacrylate, isooctyl acrylate, and isooctyl methacrylate, for example.

Further classes of compound which can be used are monofunctional acrylates and/or methacrylates of bridged cycloalkyl alcohols consisting of at least 6 carbon atoms. The cycloalkyl alcohols can also be substituted, by C-1-6 alkyl groups, halogen atoms or cyano groups, for example. Specific examples are cyclohexyl methacrylates, isobornyl acrylate, isobornyl methacrylates and 3,5-dimethyladamantyl acrylate.

In one procedure monomers are used which carry polar groups such as carboxyl radicals, sulfonic and phosphonic acid, hydroxyl radicals, lactam and lactone, N-substituted amide, N-substituted amine, carbamate, epoxy, thiol, alkoxy or cyano radicals, ethers or the like.

Moderate basic monomers are, for example, N,N-dialkyl-substituted amides, such as, for example, N,N-dimethylacrylamide, N,N-dimethylmethylmethacrylamide, N-tert-butylacrylamide, N-vinylpyrrolidone, N-vinyllactam, dimethylaminoethyl methacrylate, dimethylaminoethyl acrylate, diethylaminoethyl methacrylate, diethylaminoethyl acrylate, N-methylolmethacrylamide, N-(buthoxymethyl)methacrylamide, N-methylolacrylamide, N-isopropylacrylamide, this enumeration not being exhaustive.

Further preferred examples are hydroxyethyl acrylate, hydroxypropyl acrylate, hydroxyethyl methacrylate, hydroxypropyl methacrylate, allyl alcohol, maleic anhydride, itaconic anhydride, itaconic acid, glyceridyl methacrylate, phenoxyethyl acrylate, phenoxyethyl methacrylate, 2-butoxyethyl methacrylate, 2-butoxyethyl acrylate, cyanoethyl methacrylate, cyanoethyl acrylate, glyceryl methacrylate, 6-hydroxyhexyl methacrylate, vinylacetic acid, tetrahydrofurfuryl acrylate, β-acryloyloxypropionic acid, trichloroacrylic acid, fumaric acid, crotonic acid, aconitic acid, and dimethylacrylic acid, this enumeration not being exhaustive.

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In one further very preferred procedure use is made as monomers of vinyl esters, vinyl ethers, vinyl halides, vinylidene halides, and vinyl compounds having aromatic rings and heterocycles in α -position. Here again, mention may be made, nonexclusively, of some examples: vinyl acetate, vinylformamide, vinylpyridine, ethyl vinyl ether, vinyl chloride, vinylidene chloride, and acrylonitrile.

Moreover, in a further procedure, use is made of photoinitiators having a copolymerizable double bond. Suitable photoinitiators include Norrish I and II photoinitiators. Examples include benzoin acrylate and an acrylated benzophenone from UCB (Ebecryl P 36®). In principle it is possible to copolymerize any photoinitiators which are known to the skilled worker and which are able to crosslink the polymer by way of a free-radical mechanism under UV irradiation. An overview of possible photoinitiators for use, which can be functionalized with a double bond, is given in Fouassier: "Photoinitiation, Photopolymerization and Photocuring: Fundamentals and Applications", Hanser-Verlag, Munich 1995. Supplementarily use is made of Carroy et al. in "Chemistry and Technology of UV and EB Formulation for Coatings, Inks and Paints", Oldring (ed.), 1994, SITA, London.

In another preferred procedure the comonomers described are admixed with monomers which possess a high static glass transition temperature. Suitable components include aromatic vinyl compounds, an example being styrene, in which the aromatic nuclei consist preferably of C₄ to C₁₈ units and may also include heteroatoms. Particularly preferred examples are 4-vinylpyridine, N-vinylphthalimide, methylstyrene, 3,4-dimethoxystyrene, 4-vinylbenzoic acid, benzyl acrylate, benzyl methacrylate, phenyl acrylate, phenyl methacrylate, t-butylphenyl methacrylate,

4-biphenylyl acrylate, 4-biphenylyl methacrylate, 2-naphthyl acrylate, 2-naphthyl methacrylate, and mixtures of these monomers, this enumeration not being exhaustive.

Additionally it is a constituent of the inventive PSA that the PSA has a shrinkback, the shrinkback as determined by test B (shrinkback measurement in the free film) being at least 3%. In preferred developments PSAs are used for which the shrinkback is at least 30%, very preferably at least 50%.

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Additionally a constituent of the inventive PSA is the addition of an electrically conductive compound. In one preferred version, therefore, electrically conductive filler materials are used. Such materials include — without being restricted by this enumeration — metal particles, metal powders, metal beads, metal fibers, the metals used being, for example, nickel, gold, silver, iron, lead, tin, zinc, stainless steel, bronze and copper or nickel coatings on copper particles, on nickel particles, on polymer beads or particles, or glass microbeads. Additionally useful, for example, are lead/tin alloys with different compositions, such as are supplied, for example, by Sherrit Gordon, Ltd.

In a further embodiment of the invention, electrically conductive polymers are added, such as, for example, polythiophene, substituted polythiophenes, polyethylenedioxythiophenes, polyaniline, substituted polyanilines, polyparaphenylene, substituted polyparaphenylenes, polypyrrole, substituted polypyrroles, polyacetylenes, substituted polyphenyl sulfides, substituted polyphenyl sulfides, polyfurans, substituted polyfurans, polyalkylfluorene, substituted polyalkylfluorenes, and mixtures of the abovementioned polymers. To enhance the conductivity it is possible to add what are called dopants. Here it is possible to use various metal salts or Lewis acid or electrophiles. Examples, making no claim to completeness, are p-toluenesulfonic acid or camphorsulfonic acid. Further electrically conductive polymers include polyvinylbenzyl-trimethylammonium chloride and similar compounds, cited in US 5,061,294.

In a further preferred embodiment of the invention the diameter of the electrically conductive fillers is lower than the layer thickness of the PSA. In one preferred embodiment dispersions from ORMECON are used. Depending on dopant and chemical composition, the electrically conductive polymers added possess a conductivity of between 1 and 500 S/cm.

In a further embodiment, electrically conductive materials used can be carbon compounds, such as C-60, for example. With these compounds as well it is possible to obtain an improvement in electrical conductivity by targeted doping.

Moreover, however, it is also possible as electrically conductive substances to use hygroscopic salts, which are described in US 4,973,338.

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Electrically conductive substances are added at up to 50% percent by weight, based on the poly(meth)acrylate. In a preferred embodiment the fraction is 30% by weight based on the poly(meth)acrylate. The fraction is chosen in accordance with the desired electrical conductivity to be achieved. However, the fraction ought not to exceed an amount such that the PSA loses the pressure-sensitive adhesion properties.

For further development it is possible to admix resins to the PSAs. As tackifying resins for addition it is possible without exception to use all existing tackifier resins and those described in the literature. Representatives that may be mentioned include pinene resins, indene resins and rosins, their disproportionated, hydrogenated, polymerized, and esterified derivatives and salts, the aliphatic and aromatic hydrocarbon resins, terpene resins and terpene-phenolic resins, and also C5, C9, and other hydrocarbon resins. Any desired combinations of these and further resins may be used in order to adjust the properties of the resultant adhesive in accordance with requirements. Generally speaking it is possible to employ any resins which are compatible (soluble) with the polyacrylate in question: in particular, reference may be made to all aliphatic, aromatic and alkylaromatic hydrocarbon resins, hydrocarbon resins based on single monomers, hydrogenated hydrocarbon resins, functional hydrocarbon resins, and natural resins. Express reference may be made to the depiction of the state of the art in the "Handbook of Pressure Sensitive Adhesive Technology" by Donatas Satas (van Nostrand, 1989).

In addition it is possible optionally to add plasticizers, further fillers (such as, for example, fibers, carbon black, zinc oxide, chalk, solid or hollow glass beads, microbeads made of other materials, silica, silicates), nucleators, expandants, compounding agents and/or aging inhibitors, in the form of, for example, primary and secondary antioxidants or in the form of light stabilizers.

In addition it is possible to admix crosslinkers and crosslinking promoters. Examples of suitable crosslinkers for electron beam crosslinking and UV crosslinking include

difunctional or polyfunctional acrylates, difunctional or polyfunctional isocyanates (including those in blocked form), and difunctional or polyfunctional epoxides.

For optional crosslinking with UV light it is possible to add UV-absorbing photoinitiators to the PSAs. Useful photoinitiators whose use is very effective are benzoin ethers, such as benzoin methyl ether and benzoin isopropyl ether, substituted acetophenones, such as 2,2-diethoxyacetophenone (available as Irgacure 651° from Ciba Geigy $^{\circ}$), 2,2-dimethoxy-2-phenyl-1-phenylethanone, dimethoxyhydroxyacetophenone, substituted α -ketols, such as 2-methoxy-2-hydroxypropiophenone, aromatic sulfonyl chlorides, such as 2-naphthylsulfonyl chloride, and photoactive oximes, such as 1-phenyl-1,2-propanedione 2-(O-ethoxycarbonyl)oxime, for example.

The abovementioned photoinitiators and others which can be used, and also others of the Norrish I or Norrish II type, can contain the following radicals: benzophenone, acetophenone, benzil, benzoin, hydroxyalkylphenone, phenyl cyclohexyl ketone, anthraquinone, trimethylbenzoylphosphine oxide, methylthiophenylmorpholine ketone, aminoketone, azobenzoin, thioxanthone, hexaarylbisimidazole, triazine, or fluorenone, it being possible for each of these radicals to be additionally substituted by one or more halogen atoms and/or by one or more alkyloxy groups and/or by one or more amino groups or hydroxy groups. A representative overview is given by Fouassier: "Photoinitiation, Photopolymerization and Photocuring: Fundamentals and Applications", Hanser-Verlag, Munich 1995. For further details it is possible to consult Carroy et al. in "Chemistry and Technology of UV and EB Formulation for Coatings, Inks and Paints", Oldring (ed.), 1994, SITA, London.

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Preparation processes for the inventive PSAs

For the polymerization the monomers are chosen such that the resultant polymers can be used at room temperature or higher temperatures as PSAs, particularly such that the resulting polymers possess pressure sensitive adhesion properties in accordance with the "Handbook of Pressure Sensitive Adhesive Technology" by Donatas Satas (van Nostrand, New York 1989).

In order to achieve a preferred polymer glass transition temperature T_g of $\leq 25^{\circ}$ C for PSAs it is very preferred, in accordance with the comments made above, to select the monomers in such a way, and to choose the quantitative composition of the monomer

mixture advantageously in such a way as to result in the desired T_g for the polymer in accordance with the *Fox* equation (E1) (cf. T.G. Fox, Bull. Am. Phys. Soc. 1 (1956) 123).

$$\frac{1}{T_{g}} = \sum_{n} \frac{w_{n}}{T_{g,n}} \tag{E1}$$

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In this equation, n represents the serial number of the monomers used, w_n the mass fraction of the respective monomer n (% by weight) and $T_{g,n}$ the respective glass transition temperature of the homopolymer of each of the monomers n, in K.

For the preparation of the poly(meth)acrylate PSAs it is advantageous to carry out conventional free-radical polymerizations. For the polymerizations which proceed free-radically it is preferred to employ initiator systems which also contain further free-radical initiators for the polymerization, especially thermally decomposing, free-radical-forming azo or peroxo initiators. In principle, however, all customary initiators which are familiar to the skilled worker for acrylates are suitable. The production of C-centered radicals is described in Houben Weyl, Methoden der Organischen Chemie, Vol. E 19a, pp. 60 – 147. These methods are employed, preferentially, in analogy.

Examples of free-radical sources are peroxides, hydroperoxides, and azo compounds; some nonlimiting examples of typical free-radical initiators that may be mentioned here include potassium peroxodisulfate, dibenzoyl peroxide, cumene hydroperoxide, cyclohexanone peroxide, di-t-butyl peroxide, azodiisobutyronitrile, cyclohexylsulfonyl acetyl peroxide, diisopropyl percarbonate, t-butyl peroctoate, and benzpinacol. In one very preferred version the free-radical initiator used is 1,1'-azobis(cyclohexane-carbonitrile) (Vazo 88TM from DuPont) or azodiisobutyronitrile (AIBN).

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The electrically conductive materials can be admixed to the monomers before the polymerization and/or after the end of the polymerization.

The average molecular weights M_w of the PSAs formed in the free-radical polymerization are very preferably chosen such that they are situated within a range of 200 000 to 4 000 000 g/mol; specifically for further use as electrically conductive hot-melt PSAs with resilience, PSAs are prepared which have average molecular weights M_w of 400 000 to 1 400 000 g/mol. The average molecular weight is determined by size exclusion chromatography (GPC) or matrix-assisted laser desorption/ionization coupled with mass spectrometry (MALDI-MS).

The polymerization may be conducted without solvent, in the presence of one or more organic solvents, in the presence of water, or in mixtures of organic solvents and water. The aim is to minimize the amount of solvent used. Suitable organic solvents are straight alkanes (e.g. hexane, heptane, octane, isooctane), aromatic hydrocarbons (e.g. benzene, toluene, xylene), esters (e.g. ethyl, propyl, butyl or hexyl acetate), halogenated hydrocarbons (e.g. chlorobenzene), alkanols (e.g. methanol, ethanol, ethylene glycol, ethylene glycol monomethyl ether), and ethers (e.g. diethyl ether, dibutyl ether) or mixtures thereof. A water-miscible or hydrophilic cosolvent may be added to the aqueous polymerization reactions in order to ensure that the reaction mixture is present in the form of a homogeneous phase during monomer conversion. Cosolvents which can be used with advantage for the present invention are chosen from the following group, consisting of aliphatic alcohols, glycols, ethers, glycol ethers, pyrrolidines, N-alkylpyrrolidinones, N-alkylpyrrolidones, polyethylene glycols, polypropylene glycols, amides, carboxylic acids and salts thereof, esters, organic sulfides, sulfoxides, sulfones, alcohol derivatives, hydroxy ether derivatives, amino alcohols, ketones and the like, and also derivatives and mixtures thereof.

The polymerization time - depending on conversion and temperature - is between 2 and 72 hours. The higher the reaction temperature which can be chosen, i.e., the higher the thermal stability of the reaction mixture, the shorter can be the chosen reaction time.

As regards initiation of the polymerization, the introduction of heat is essential for the thermally decomposing initiators. For these initiators the polymerization can be initiated by heating to from 50 to 160°C, depending on initiator type.

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For the preparation it can also be of advantage to polymerize the acrylate PSAs without solvent. A particularly suitable technique for use in this case is the prepolymerization technique. Polymerization is initiated with UV light but taken only to a low conversion of about 10 - 30%. The resulting polymer syrup can then be welded, for example, into films (in the simplest case, ice cubes) and then polymerized through to a high conversion in water. These pellets can subsequently be used as acrylic hot-melt adhesives, it being particularly preferred to use, for the melting operation, film materials which are compatible with the polyacrylate. For this preparation method as well it is possible to add the thermally conductive materials before or after the polymerization.

Another advantageous preparation process for the poly(meth)acrylate PSAs is that of anionic polymerization. In this case the reaction medium used preferably comprises inert solvents, such as aliphatic and cycloaliphatic hydrocarbons, for example, or else aromatic hydrocarbons.

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The living polymer is in this case generally represented by the structure $P_L(A)$ -Me, where Me is a metal from group I, such as lithium, sodium or potassium, and $P_L(A)$ is a growing polymer from the acrylic monomers. The molar mass of the polymer under preparation is controlled by the ratio of initiator concentration to monomer concentration. Examples of suitable polymerization initiators include n-propyllithium, n-butyllithium, sec-butyllithium, 2-naphthyllithium, cyclohexyllithium, and octyllithium, though this enumeration makes no claim to completeness. Furthermore, initiators based on samarium complexes are known for the polymerization of acrylates (Macromolecules, 1995, 28, 7886) and can be used here.

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It is also possible, furthermore, to employ difunctional initiators, such as 1,1,4,4-tetraphenyl-1,4-dilithiobutane or 1,1,4,4-tetraphenyl-1,4-dilithioisobutane, for example. Coinitiators can likewise be employed. Suitable coinitiators include lithium halides, alkali metal alkoxides, and alkylaluminum compounds. In one very preferred version the ligands and coinitiators are chosen so that acrylic monomers, such as n-butyl acrylate and 2-ethylhexyl acrylate, for example, can be polymerized directly and do not have to be generated in the polymer by transesterification with the corresponding alcohol.

Methods suitable for preparing polyacrylate PSAs with a narrow molecular weight distribution also include controlled free-radical polymerization methods. In that case it is preferred to use, for the polymerization, a control reagent of the general formula:

in which R and R¹, chosen independently of one another or identical, are

- branched and unbranched C₁ to C₁₈ alkyl radicals; C₃ to C₁₈ alkenyl radicals; C₃ to C₁₈ alkynyl radicals;
- C₁ to C₁₈ alkoxy radicals;

- C₃ to C₁₈ alkynyl radicals; C₃ to C₁₈ alkenyl radicals; C₁ to C₁₈ alkyl radicals substituted by at least one OH group or a halogen atom or a silyl ether;
- C₂-C₁₈ heteroalkyl radicals having at least one oxygen atom and/or one NR* group
 in the carbon chain, R* being any radical (particularly an organic radical);
- C₃-C₁₈ alkynyl radicals, C₃-C₁₈ alkenyl radicals, C₁-C₁₈ alkyl radicals substituted by at least one ester group, amine group, carbonate group, cyano group, isocyano group and/or epoxy group and/or by sulfur;
- C₃-C₁₂ cycloalkyl radicals;
- C₆-C₁₈ aryl or benzyl radicals;
- 10 hydrogen.

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Control reagents of type (I) are preferably composed of the following further-restricted compounds:

halogen atoms therein are preferably F, Cl, Br or I, more preferably Cl and Br. Outstandingly suitable alkyl, alkenyl and alkynyl radicals in the various substituents include both linear and branched chains.

Examples of alkyl radicals containing 1 to 18 carbon atoms are methyl, ethyl, propyl, isopropyl, butyl, isobutyl, t-butyl, pentyl, 2-pentyl, hexyl, heptyl, octyl, 2-ethylhexyl, t-octyl, nonyl, decyl, undecyl, tridecyl, tetradecyl, hexadecyl, and octadecyl.

Examples of alkenyl radicals having 3 to 18 carbon atoms are propenyl, 2-butenyl, 3-butenyl, isobutenyl, n-2,4-pentadienyl, 3-methyl-2-butenyl, n-2-octenyl, n-2-dodecenyl, isododecenyl, and oleyl.

Examples of alkynyl having 3 to 18 carbon atoms are propynyl, 2-butynyl, 3-butynyl, n-2-octynyl, and n-2-octadecynyl.

Examples of hydroxy-substituted alkyl radicals are hydroxypropyl, hydroxybutyl, and hydroxyhexyl.

Examples of halogen-substituted alkyl radicals are dichlorobutyl, monobromobutyl, and trichlorohexyl.

An example of a suitable C_2 - C_{18} heteroalkyl radical having at least one oxygen atom in the carbon chain is $-CH_2$ - CH_2 - CH_2 - CH_3 .

30 Examples of C_3 - C_{12} cycloalkyl radicals include cyclopropyl, cyclopentyl, cyclohexyl, and trimethylcyclohexyl.

Examples of C₆-C₁₈ aryl radicals include phenyl, naphthyl, benzyl, 4-tert-butylbenzyl, and other substituted phenyls, such as ethyl, toluene, xylene, mesitylene, isopropylbenzene, dichlorobenzene or bromotoluene.

35 The above enumerations serve only as examples of the respective groups of compounds, and make no claim to completeness.

Other compounds which can be used as control reagents include those of the following types:

where R², again independently from R and R¹, may be selected from the group recited above for these radicals.

In the case of the conventional 'RAFT' process, polymerization is generally carried out only up to low conversions (WO 98/01478 A1) in order to produce very narrow molecular weight distributions. As a result of the low conversions, however, these polymers cannot be used as PSAs and in particular not as hot-melt PSAs, since the high fraction of residual monomers adversely affects the technical adhesive properties; the residual monomers contaminate the solvent recyclate in the concentration operation; and the corresponding self-adhesive tapes would exhibit very high outgassing behavior. In order to circumvent this disadvantage of low conversions, the polymerization in one particularly preferred procedure is initiated two or more times.

As a further controlled free-radical polymerization method it is possible to carry out nitroxide-controlled polymerizations. For free-radical stabilization, in a favorable procedure, use is made of nitroxides of type (Va) or (Vb):

where R^3 , R^4 , R^5 , R^6 , R^7 , R^8 , R^9 , and R^{10} independently of one another denote the following compounds or atoms:

i) halides, such as chlorine, bromine or iodine, for example,

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- ii) linear, branched, cyclic, and heterocyclic hydrocarbons having 1 to 20 carbon atoms, which may be saturated, unsaturated or aromatic,
- iii) esters –COOR¹¹, alkoxides –OR¹² and/or phosphonates –PO(OR¹³)₂, where R¹¹, R¹² or R¹³ stand for radicals from group ii).
- Compounds of type (Va) or (Vb) can also be attached to polymer chains of any kind (primarily such that at least one of the abovementioned radicals constitutes a polymer chain of this kind) and may therefore be used for the synthesis of polyacrylate PSAs.

 More preferred are controlled regulators for the polymerization of compounds of the following type:
- 10 2,2,5,5-tetramethyl-1-pyrrolidinyloxyl (PROXYL), 3-carbamoyl-PROXYL, 2,2-dimethyl-4,5-cyclohexyl-PROXYL, 3-oxo-PROXYL, 3-hydroxylimine-PROXYL, 3-aminomethyl-PROXYL, 3-methoxy-PROXYL, 3-t-butyl-PROXYL, 3,4-di-t-butyl-PROXYL
 - 2,2,6,6-tetramethyl-1-piperidinyloxy pyrrolidinyloxyl (TEMPO), 4-benzoyloxy-TEMPO,
 4-methoxy-TEMPO,
 4-chloro-TEMPO,
 4-hydroxy-TEMPO,
 4-amino-TEMPO,
 2,2,6,6,-tetraethyl-1-piperidinyloxyl,
 2,2,6-trimethyl-6-ethyl-1-piperidinyloxyl
 - N-tert-butyl 1-phenyl-2-methylpropyl nitroxide
 - N-tert-butyl 1-(2-naphthyl)-2-methylpropyl nitroxide
 - N-tert-butyl 1-diethylphosphono-2,2-dimethylpropyl nitroxide
- 20 N-tert-butyl 1-dibenzylphosphono-2,2-dimethylpropyl nitroxide
 - N-(1-phenyl-2-methylpropyl) 1-diethylphosphono-1-methylethyl nitroxide
 - · di-t-butyl nitroxide

- diphenyl nitroxide
- t-butyl t-amyl nitroxide.
- A series of further polymerization methods in accordance with which the PSAs can be prepared by an alternative procedure can be chosen from the prior art:

 US 4,581,429 A discloses a controlled-growth free-radical polymerization process which uses as its initiator a compound of the formula R'R"N-O-Y, in which Y is a free-radical species which is able to polymerize unsaturated monomers. In general, however, the reactions have low conversion rates. A particular problem is the polymerization of acrylates, which takes place only with very low yields and molar masses. WO 98/13392 A1 describes open-chain alkoxyamine compounds which have a symmetrical substitution pattern. EP 735 052 A1 discloses a process for preparing thermoplastic elastomers having narrow molar mass distributions. WO 96/24620 A1 describes a polymerization process in which very specific free-radical compounds, such

as phosphorus-containing nitroxides based on imidazolidine, for example, are employed. WO 98/44008 A1 discloses specific nitroxyls based on morpholines, piperazinones, and piperazinediones. DE 199 49 352 A1 describes heterocyclic alkoxyamines as regulators in controlled-growth free-radical polymerizations. Corresponding further developments of the alkoxyamines or of the corresponding free nitroxides improve the efficiency for the preparation of polyacrylates (Hawker, paper to the National Meeting of the American Chemical Society, Spring 1997; Husemann, paper to the IUPAC World-Polymer Meeting 1998, Gold Coast).

10 As a further controlled polymerization method, atom transfer radical polymerization (ATRP) can be used advantageously to synthesize the polyacrylate PSAs, in which case use is made preferably as initiator of monofunctional or difunctional secondary or tertiary halides and, for abstracting the halide(s), of complexes of Cu, Ni, Fe, Pd, Pt, Ru, Os, Rh, Co. Ir. Ag or Au (EP 0 824 111 A1; EP 826 698 A1; EP 824 110 A1; EP 841 346 A1; EP 850 957 A1). The various possibilities of ATRP are further described in 15 US 5,945,491 A, US 5,854,364 A and US 5,789,487 A.

Orientation, coating processes, treatment of the carrier material with the electrically conductive PSA

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In order to produce oriented PSAs the polymers described above are coated preferably as hotmelt systems (i.e., from the melt). For the production process it may therefore be necessary to remove the solvent from the PSA. In principle it is possible here to use any of the techniques known to the skilled worker. One very preferred technique is that of concentration using a single-screw or twin-screw extruder. The twin-screw extruder may be operated corotatingly or counterrotatingly. The solvent or water is distilled off preferably by way of two or more vacuum stages. Moreover, counterheating is carried out depending on the distillation temperature of the solvent. The residual solvent fractions are preferably < 1%, more preferably < 0.5% and very preferably < 0.2%. The hotmelt is processed further from the melt.

Orientation within the PSA is produced in the course of coating by means of the coating

process. For coating as a hotmelt, and hence also for orientation, it is possible to employ different coating techniques. In one version the electrically conductive PSAs are coated by a roll coating process, and the orientation is produced by drawing. Various roll coating techniques are described in the "Handbook of Pressure Sensitive Adhesive Technology" by Donatas Satas (van Nostrand, New York 1989). In another version the orientation is achieved by coating via a melt die. A distinction can be made here between the contact process and the noncontact process. Orientation of the electrically conductive PSA here can be produced on the one hand within the coating die, by virtue of the die design, or else following emergence form the die, by a drawing operation. The orientation is freely adjustable. The draw ratio can be controlled, for example, by the width of the die gap. Drawing occurs whenever the layer thickness of the PSA film on the carrier material to be coated is less than the width of the die gap.

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In another preferred process the orientation is achieved by extrusion coating. Extrusion coating is preferably performed using an extrusion die. The extrusion dies used may originate with advantage from one of the following three categories: T-dies, fishtail dies, and coathanger dies. The individual types differ in the design of their flow channel. Through the form of the extrusion die it is likewise possible to produce an orientation within the hotmelt PSA. Additionally, here, in analogy to melt die coating, it is likewise possible to obtain an orientation following emergence from the die, by drawing the PSA tape film.

In order to produce oriented (meth)acrylate PSAs it is particularly preferred to carry out coating onto a carrier using a coathanger die, and specifically in such a way that a polymer layer is formed on the carrier by means of a movement of die relative to carrier. The time which elapses between coating and crosslinking is advantageously small. In one preferred procedure, crosslinking is carried out after less than 60 minutes; in a more preferred procedure, after less than 3 minutes; and, in a very preferred procedure, in an inline process, after less than 5 seconds.

The carrier material treated with electrically conductive PSA may be a single-sided or a double-sided adhesive tape.

In one very preferred version, transfer tapes are produced. Examples of suitable carrier material includes all siliconized or fluorinated films having a release effect. Film materials that may be mentioned here, mainly by way of example, include BOPP, MOPP, PET, PVC, PU, PE, PE/EVA, EPDM, PP and PE. For transfer tapes, moreover, it is also possible to use release papers (glassine papers, kraft papers, polyolefinically coated papers).

Where the carrier material remains in the PSA (in the form of a carrier film, for example) it is preferred to use a carrier material which likewise possesses a high high electrical conductivity. For this case it is possible, for example, to use metal or metallized films or metal-doped films.

Particularly preferred films are composed, without this enumeration making any claim to completeness, of aluminum, copper, stainless steel, or metal alloys. In another embodiment a polymeric carrier material is chosen, such as PE, PP, polyimide, PET, PVC, PU or nylon, for example, and is provided on one or both sides with a metal layer. Metals which can be used include, for example, aluminum, chromium, nickel, copper, nickel alloys, silver, gold or mixtures of these. In one preferred technique these metals are applied to the films by means of the sputtering method, with very low layer thicknesses.

In addition, however, it is also possible to use metallized woven carrier materials. Examples of such are given for example in US 5,939,190.

The best orientation effects are obtained by deposition onto a cold surface. Consequently the carrier material during coating should be cooled directly by means of a roll. The roll can be cooled by a liquid film/contact film from the outside or inside, or by a coolant gas. The coolant gas may likewise be used to cool the PSA emerging from the coating die. In one preferred procedure the roll is wetted with a contact medium, which is then located between the roll and the carrier material. Preferred embodiments for the implementation of such a technique are described later on below.

For this process it is possible to use both a melt die and an extrusion die. In one very preferred procedure the roll is cooled to room temperature, and in an extremely preferred procedure to temperatures below 10°C. The roll ought to rotate as well.

In a further procedure as part of this production process, the roll is used, moreover, for crosslinking of the oriented PSA.

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UV crosslinking is effected by irradiation with shortwave ultraviolet radiation in a wavelength range from 200 to 400 nm, depending on the UV photoinitiator used, especially using high-pressure or medium-pressure mercury lamps at an output of 80 to 240 W/cm. The irradiation intensity is adapted to the respective quantum yield of the UV photoinitiator, the degree of crosslinking to be brought about, and the extent of the orientation.

Moreover, in one preferred version, it is possible to crosslink the electroconductive and oriented PSAs using electron beams. Typical irradiation equipment which may be used includes linear cathode systems, scanner systems and segmented cathode systems, where electron-beam accelerators are concerned. An extensive description of the state of the art and the most important process parameters are found in Skelhorne, Electron Beam Processing, in Chemistry and Technology of UV and EB formulation for Coatings, Inks and Paints, Vol. 1, 1991, SITA, London. The typical accelerator voltages are situated in the range between 50 kV and 500 kV, preferably 80 kV and 300 kV. The scatter doses employed range between 5 to 150 kGy, in particular between 20 and 100 kGy.

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It is also possible to employ both crosslinking methods, or other methods which permit high-energy irradiation.

In a further preferred production process, the electroconductive and oriented PSAs are coated onto a roll provided with a contact medium. As a result of the contact medium it is possible in turn to carry out very rapid cooling of the PSA. Advantageously, lamination is then carried out onto the carrier material later.

Furthermore, as the contact medium it is also possible to use a material which has the capacity to bring about contact between the PSA and the roll surface, in particular a material which fills the cavities between carrier material and roll surface (unevennesses in the roll surface, bubbles, for example). In order to implement this technology, a rotating chill roll is coated with a contact medium. In one preferred procedure the contact medium chosen is a liquid, such as water, for example.

Examples of appropriate additives to water as the contact medium include alkyl alcohols such as ethanol, propanol, butanol and hexanol, without wishing to be restricted in the selection of the alcohols as a result of these examples. Also highly advantageous are, in particular, longer-chain alcohols, polyglycols, ketones, amines, carboxylates, sulfonates and the like. Many of these compounds lower the surface tension or raise the conductivity.

A lowering of the surface tension may also be achieved by adding small amounts of nonionic and/or anionic and/or cationic surfactants to the contact medium. The most simple way of achieving this is by using commercial washing compositions or soap solutions, preferably in a concentration of a few g/l in water, as the contact medium. Particularly suitable compounds are special surfactants which can be used even at a low

concentration. Examples thereof include sulfonium surfactants (e.g., β-di(hydroxyl-alkyl)sulfonium salt), and also, for example, ethoxylated nonylphenylsulfonic acid ammonium salts or block copolymers, especially diblocks. Here, reference may be made in particular to the state of the art under "surfactants" in Ullmann's Encyclopedia of Industrial Chemistry, Sixth Edition, 2000 Electronic Release, Wiley-VCH, Weinheim 2000.

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As contact media it is possible to use the aforementioned liquids, even without the addition of water, in each case alone or in combination with one another.

In order to improve the properties of the contact medium (for example, to increase the shearing resistance, reduce the transfer of surfactants or the like to the liner surface, and thus improved cleaning possibilities for the end product), salts, gels and similar viscosity-enhancing additives may also be added with advantage to the contact medium and/or to the adjuvants employed.

Furthermore, the roll can be macroscopically smooth or can have a surface with a low level of structuring. It has been found appropriate for the roll to possess a surface structure, in particular a surface roughening. This allows wetting by the contact medium to be improved.

The coating process runs particularly well if the roll is temperature-controllable, preferably within a range from -30°C to 200°C, very preferably from 5°C to 25°C.

The contact medium is preferably applied to the roll. A second roll, which takes up the contact medium, may be used for continuous wetting of the coating roll. It is, however, also possible to carry out contactless application, by spraying, for example.

For the variant of the production process where the roll is employed simultaneously for use, for example, with electron beams it is common to use a grounded metal roll which absorbs the incident electrons and the X-radiation that is formed in the process.

In order to prevent corrosion, the roll is commonly coated with a protective coat. This coat is preferably selected such that it is wetted effectively by the contact medium. In general, the surface is conductive. It may also be more advantageous, however, to coat it with one or more coats of insulating or semiconducting material.

Where a liquid is used as the contact medium, one outstanding procedure possible is to run a second roll, advantageously having a wettable or absorbent surface, through a bath containing the contact medium, said roll then becoming wetted by or impregnated with the contact medium and applying a film of said contact medium by contact with the roll.

In one preferred procedure the PSA is coated directly on the contact medium roll, and crosslinked. For this purpose it is possible in turn to use the methods and equipment described for UV crosslinking and EB crosslinking. Then, following crosslinking, the electrically conductive and oriented PSA is transferred to a carrier material. The carrier materials already stated may be used.

The characterization of the orientation within the electrically conductive PSAs is dependent on the coating process. The orientation can be controlled, for example, by the die temperature and coating temperature and also by the molecular weight of the polymer.

The degree of orientation is freely adjustable through the die gap width. The thicker the PSA film extruded from the coating die, the greater the extent to which the adhesive can be drawn to a relatively thin PSA film on the carrier material. This drawing operation may be freely adjusted not only by the freely adjustable die width but also by the web speed of the decreasing carrier material.

The orientation of the adhesive mass can additionally be measured with a polarimeter, by infrared dichroism, or using X-ray scattering. It is known that in many cases the orientation in acrylate PSAs in the uncrosslinked state is retained for only a few days. During rest or storage, the system relaxes and loses its preferential direction. As a result of crosslinking after coating, this effect can be strengthened significantly. The relaxation of the oriented polymer chains converges toward zero, and the oriented PSAs can be stored for a very long period of time without loss of their preferential direction.

In one preferred method the extent of the orientation is determined by measuring the shrinkback in the free film (see test B).

Besides the processes described, the orientation may also be produced after coating. In that case, then, a stretchable carrier material is preferably used, with the PSA then being drawn during stretching. In this case it is also possible to use PSAs coated conventionally from solution or water. In one preferred procedure, then, this drawn PSA is in turn crosslinked with actinic radiation.

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<u>Use</u>

The invention further provides for the use of the electroconductive and oriented PSAs for bonding components in the electrical and electronics industry. In one preferred embodiment the inventive PSAs are used as transfer tapes. In this case the release paper is removed in order to bond electrically conductive substances. If very close conductor tracks are bonded in parallel, the direction of bonding is chosen such that the inventive electroconductive PSA possesses a resilience in the direction of the next parallel conductor track. In this way it is possible to avoid short circuits, since in contrast to conventional electrically conductive PSAs the PSA does not flow out in this direction.

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A further advantage are electrically conductive PSA diecuts, which are particularly easy to produce and which even during bonding are very dimensionally stable and therefore are suitable very effectively for bonding very small electrical parts.

A further advantage of the electrically conductive and oriented PSAs lies in the reversibility. As a result of the orientation, the inventive PSAs can be stretched in the oriented direction, leading in turn to a decrease in bond strength and in tack. By this means it is possible for electroconductive substances bonded with the inventive PSA to be parted from one another again.

In a further embodiment the inventive PSA possesses anisotropic electroconductive properties. As a result of the orientation of the polymer chains, the electrically conductive filler materials are pulled apart in one preferential direction and lose contact with one another. As a result of this process the electrical conductivity in the direction of orientation is lowered, so that the PSAs and hence also the corresponding PSA tapes likewise have anisotropic electrical conductivities.

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Examples

The invention is illustrated below, without restriction as to its general nature, by means of examples and experiments.

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The following test methods were employed for investigating the samples:

Gel permeation chromatography GPC (test A)

The average molecular weight M_w and the polydispersity PD were determined by gel permeation chromatography. The eluent used was THF containing 0.1% by volume trifluoroacetic acid. Measurement took place at 25°C. The precolumn used was PSS-SDV, 5 μ , 10³ Å, ID 8.0 mm \times 50 mm. Separation was carried out using the columns

PSS-SDV, 5 μ , 10³ and also 10⁵ and 10⁶ each with ID 8.0 mm \times 300 mm. The sample concentration was 4 g/I, the flow rate 1.0 ml per minute. Measurement was made against PMMA standards.

5 Measurement of the shrinkback (test B)

Strips with a width of at least 30 mm and a length of 20 cm were cut parallel to the coating direction of the hotmelt. At application rates of 100 g/m², 4 strips each were laminated to one another, and, at 50 g/m², 8 strips were laminated to one another, so as to give comparable layer thicknesses. The specimen obtained in this way was then cut to a width of exactly 20 mm and was overstuck at each end with paper strips, with a spacing of 15 cm. The test specimen thus prepared was then suspended vertically at RT and the change in length was monitored over time until no further contraction of the sample could be found. The initial length reduced by the final value was then reported, relative to the initial length, as the shrinkback, in percent.

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To measure the orientation after a longer time, the coated and oriented PSAs were stored in the form of swatches for a prolonged period and then analyzed.

Measurement of the contact resistance (test C)

The electrical conductivity is measured via the electrical contact resistance by the 4-wire method. For the investigation, measurement was carried out against aluminum and against copper. In each case a PSA film 50 μm thick was bonded to a solid copper plate. Prior to the measurement, the plates had been roughened with sandpaper and cleaned with ethanol. The foil bonded was a copper foil. The measurement area was 2.54 × 2.54 cm.

180° bond strength test (test D)

A strip, 20 mm wide, of an acrylate PSA coated onto a polyester or siliconized release paper was applied to steel plates. Depending on direction and drawing, longitudinal or transverse specimens were bonded to the steel plate. The PSA strip was pressed onto the substrate twice using a 2 kg weight. Immediately thereafter the adhesive tape was peeled from the substrate at 30 mm/min and at an angle of 180°. The steel plates were washed twice with acetone and once with isopropanol. The results of measurement are reported in N/cm and are averaged from three measurements. All measurements were carried out at room temperature under controlled-climate conditions.

Electroconductive materials used:

Silver-coated nickel particles:

20 – 40 µm diameter, available from Potter Industries.

5 Nickel particles:

Diameter greater than 10 µm, available from Novamet, Inc.

Sample preparation

10 Polymer 1

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A 200 L reactor conventional for free-radical polymerizations was charged with 2400 g of acrylamide, 64 kg of 2-ethylhexyl acrylate, 6.4 kg of N-isopropylacrylamide and 53.3 kg of acetoneisopropanol (95:5). After nitrogen gas had been passed through the reactor for 45 minutes with stirring, the reactor was heated to 58° C and 40 g of 2,2'-azoisobutyronitrile (AIBN) were added. The external heating bath was then heated to 75°C and the reaction was carried out constantly at this external temperature. After a reaction time of 1 h a further 40 g of AIBN were added. After 5 h and 10 h, dilution was carried out each time with 15 kg of acetone/isopropanol (95:5). After 6 h and 8 h, 100 g portions of dicyclohexyl peroxydicarbonate (Perkadox 16° , Akzo Nobel) each in solution of 800 g of acetone were added. After a reaction time of 24 h the reaction was terminated and the batch cooled to room temperature. Determination of the molecular weight by test A gave an $M_{\rm w} = 754\,000$ g/mol with a polydispersity $M_{\rm w}/M_{\rm n} = 5.3$.

Polymer 2

A 200 L reactor conventional for free-radical polymerizations was charged with 1200 g of acrylamide, 74 kg of 2-ethylhexyl acrylate, 4.8 kg of N-isopropylacrylamide and 53.3 kg of acetoneisopropanol (95:5). After nitrogen gas had been passed through the reactor for 45 minutes with stirring, the reactor was heated to 58°C and 40 g of 2,2'-azoisobutyronitrile (AIBN) were added. The external heating bath was then heated to 75°C and the reaction was carried out constantly at this external temperature. After a reaction time of 1 h a further 40 g of AIBN were added. After 5 h and 10 h, dilution was carried out each time with 15 kg of acetone/isopropanol (95:5). After 6 h and 8 h, 100 g portions of dicyclohexyl peroxydicarbonate (Perkadox 16®, Akzo Nobel) each in solution of 800 g of acetone were added. After a reaction time of 24 h the reaction was terminated and the batch cooled to room temperature.

Determination of the molecular weight by test A gave an M_w = 812 000 g/mol with a polydispersity M_w/M_n = 5.8.

Example 1:

5 Polymer 1 was blended with 20% by weight of silver-coated nickel particles, based on the polymer fraction.

Example 2:

Polymer 1 was blended with 30% by weight of silver-coated nickel particles, based on the polymer fraction.

Example 3:

Polymer 2 was blended with 20% by weight of nickel particles, based on the polymer fraction.

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Example 4:

Polymer 2 was blended with 30% by weight of nickel particles, based on the polymer fraction.

20 i) Production of specimens for determining the shrinkback

The PSAs in solution were concentrated on a Bersdorff concentrating extruder with a throughput of approximately 40 kg/h at a temperature of approximately 115°C. Following concentration, the residual solvent fraction was less than 0.5% by weight. The composition was then coated onto a 12 μ m PET film coated beforehand with 1.5 g/m² silicone (polydimethylsiloxane), application of the composition taking place through a coathanger extrusion die with a die gap of 300 μ m and a coating width of 33 cm, at a defined coating temperature (composition temperature) and a web speed of 10 m/min. For an application rate of 100 g/m² (PSA layer approximately 100 μ m thick) a draw ratio of 3:1 was set, and for an application rate of 50 g/m² (PSA layer approximately 50 μ m thick) a draw ratio of 6:1 was set.

The siliconized PET film is passed over a corotating steel roller which is cooled to 5°C. At the point of contact between the PSA film and the PET film, therefore, the PSA film is immediately cooled. The application rate was 50 or 100 g/m².

In an inline process, after a web section of approximately 5 m, the PSA tape is then crosslinked with electron beams.

For electron beam irradiation, crosslinking was carried out with an instrument from Electron Crosslinking AB, Halmstad, Sweden. The coated PSA tape was guided through under the Lenard window of the accelerator over a chill roll that is present as a standard feature. Within their radiation zone, the atmospheric oxygen was displaced by flushing with pure nitrogen. The web speed was in each case 10 m/min. Irradiation was carried out with an acceleration voltage of 200 kV.

To determine the shrinkback, test B was carried out.

10 To determine the electrical conductivity, test C was carried out. The bond strength was determined according to test D.

<u>Results</u>

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In a first step, 2 polymers were prepared, with an average molecular weight M_w of about 800 000 g/mol. These PSAs were used to produce inventive examples 1 to 4. As the electrically conductive materials, a selection was made on the one hand of a nickel particle and on the other hand of silver-coated nickel particles.

In a first analysis the degree of orientation of the individual PSAs was determined. Therefore, in the text below, the shrinkback in the free film was determined according to test method B. The measured values are summarized in table 1.

Table 1. Overview of shrinkback values determined in the free film (test B).

Example	Shrinkback in the free film (test B)
1	65%
2	70%
3	62%
4	69%

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All of the examples in table 1 exhibit a pronounced resilience. A further prerequisite for the inventive PSAs is the electrical conductivity. Below, therefore, the electrical conductivity of the individual examples was determined according to test method C. The values determined are summarized in table 2.

Example	Electrical resistance (test C) in Ω
1	< 0.75
2	< 0.5
3	< 0.75
4	< 0.5

All electrical resistances were determined with a layer thickness of 50 μ m. The materials all possessed lower electrical resistances and therefore a high electrical conductivity. By raising the electrically conductive additions to 30 weight% the electrical resistance was lowered further significantly to < 0.5 Ω .

To ascertain the adhesive properties, the bond strength to steel was determined additionally. For these measurements as well the layer thickness of the PSA was 50 μm . The values measured are listed in table 3:

Table 3: Overview of bond strengths determined according to test D

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Example	Bond strength on steel (test D) in [N/cm]
1	2.9
2	2.5
3	3.2
4	2.7

15 The values shown in table 3 make it clear that examples 1 - 4 possess pressure-sensitive adhesion properties. Through the amounts of the additive it is likewise possible to control the bond strength. High fractions of the filler material lower the bond strength.

Patent claims:

1. A method of producing a pressure-sensitive adhesive article having at least one layer of an electrically conductive pressure-sensitive adhesive, characterized in that a layer of the electrically conductive pressure-sensitive adhesive that is anisotropic at least in respect of one property is produced in a coating process by stretching, drawing or compressing, said layer possessing in at least one direction along the plane of the layer a shrinkback of at least 3% in respect of the longitudinal extent of the layer, measured on the free pressure-sensitive adhesive film.

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- 2. The method of claim 1, characterized in that the coating process is a hotmelt roll coating process, a melt diecoating process or an extrusion coating process.
- 3. The method of claim 1, characterized in that the coating process is a conventional coating process with subsequent stretching or drawing on a stretchable carrier.
 - 4. The method of any one of claims 1 to 3, characterized in that the electrically conductive pressure-sensitive adhesive is coated onto one or both sides of a sheetlike or tapelike carrier.

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- 5. The method of claim 4, characterized in that the carrier is a transfer tape, a release liner or an electrically conducting carrier material.
- 6. The method of any one of claims 1 to 5, characterized in that the pressuresensitive adhesive used is based on polyacrylate and/or polymethacrylate.
 - 7. The method of claim 6, characterized in that the pressure-sensitive adhesive is based to an extent of at least 50% by weight on at least one acrylic monomer from the group of the compounds of the following general formula:

where R_1 = H or CH_3 and the radical R_2 = H or CH_3 or is chosen from the group of the branched or unbranched, saturated alkyl groups having 2 – 30 carbon atoms and the average molecular weight M_W of the pressure-sensitive adhesive is at least 200 000 g/mol.

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8. The method of any one of claims 1 to 6, characterized in that crosslinkers, especially difunctional or polyfunctional acrylates and/or methacrylates, difunctional or polyfunctional isocyanates or difunctional or polyfunctional epoxides, have been added to the pressure-sensitive adhesive.

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9. The method of claim 8, characterized in that the pressure-sensitive adhesive is crosslinked, preferably photochemically, immediately after or during hotmelt coating.

10. The method of any one of claims 1 to 9, characterized in that electrically conductive materials, especially metal particles, metal powders, metal beads, metal fibers, the metals being in particular nickel, gold, silver and copper or the following nickel-coated particles: copper particles, nickel particles, polymer beads, polymer particles or glass microbeads or hollow glass microbeads, have been admixed to the pressure-sensitive adhesive.

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11. The method of claim 10, characterized in that the electrically conductive materials are admixed in a fraction of up to 200% by weight, preferably between 5% and 50% by weight, more preferably between 10% and 40% by weight, based on the weight of the pressure-sensitive adhesive.

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12. The method of any one of claims 1 to 11, characterized in that the electrical conductivity of the pressure-sensitive adhesive is between 1 and 500 S/cm.

- 13. The method of any one of claims 1 to 12, characterized in that the electrical conductivity is anisotropic and is lower along a plane lying in the pressure-sensitive adhesive layer than transverse to the plane of the layer, it being at least 2 S/cm in a direction transverse to the plane of the layer.
- 14. The method of any one of claims 1 to 13, characterized in that the pressuresensitive adhesive comprises further substances or additives, such as aging inhibitors,

light stabilizers, ozone protectants, fatty acids, plasticizers, nucleators, expandants, accelerators and/or fillers.

- 15. A pressure-sensitive adhesive article, in particular for bonding two electrical parts, obtainable by a method of any one of claims 1 to 14.
 - 16. The pressure-sensitive adhesive article of claim 15 in the form of a diecut.

Abstract

In a method of producing a pressure-sensitive adhesive article an electrically conductive acrylate-containing pressure-sensitive adhesive is coated within a hotmelt coating process in such a way, with stretching or drawing, onto a backing, that an anisotropic electrically conductive layer is produced which has a shrinkback of at least 3% measured on the free pressure-sensitive adhesive film. From the material it is possible with advantage to manufacture diecuts for the electrical and electronics industry.